Dimensional Analysis

Procedure to Apply the Buckingham Pi Theorem:

- 1. List the "*n*" parameters involved, starting with the dependent parameter.
- 2. Under each parameter, write the primary dimensions MLtT.
- 3. Find the rank " r " of the dimensional matrix. Typically $r =$ number of primary dimensions.
- 4. Select *r repeating parameters* from the *n* available. Avoid the *dependent variable* along with μ , c , Δp or σ . The repeating parameters must have independent units that yet include in total all the primary dimensions. The best choice is that of parameters similar to ρ , V , D .
- 5. For each of the $(n r)$ remaining parameters (called *nonrepeating*), form a nondimensional Pi parameter Π starting with the dependent variable.
- 6. Express the Pi parameter containing the dependent variable as a function of the remaining Pi parameters: $\Pi_1 = F(\Pi_2, \Pi_3, \ldots)$. Identify well-known Pi parameters, especially those that are named after famous scientists.

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\frac{\rho VL}{\mu} = \text{Re Reynolds no.} \propto \frac{\text{Inertial Force}}{\text{Viscous Force}} \text{ near solid boundaries.}
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$$
\frac{V}{c} = \sqrt{\frac{\rho V^2}{p}} = \frac{V}{\sqrt{kRT}} = M \text{ Mach no.} \propto \frac{\text{Inertial Force}}{\text{Compressibility Force}} \text{ in high speed gaseous flows.}
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$$
\frac{\omega L}{V} \text{ or } \frac{fL}{V} = St \text{ Strouhal no.} \propto \frac{\text{Time-Dependent Inertial Force}}{\text{Time-Independent Inertial Force}} \text{unsteady/oscillatory flows.}
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$$
L \sqrt{\frac{\omega}{\nu}} = \lambda \text{ Stokes/Womersley no.} \propto \frac{\text{Time-Dependent Inertial Force}}{\text{Viscous Force}} \text{unsteady flows near walls.}
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\frac{V}{\sqrt{gL}} \text{ or } \frac{V^2}{gL} = Fr \text{ Froude no.} \propto \frac{\text{Inertial Force}}{\text{Gravitational Force}} \text{ in free-surface flows.}
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\frac{\rho V^2 L}{\sigma} = We \text{ Weber no.} \propto \frac{\text{Inertial Force}}{\text{Surface Tension Force}} \text{ in capillary flows, droplets, ripple waves.}
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$$
\frac{\mu V}{\sigma} = Ca \text{ Capillarity no.} \propto \frac{\text{Viscous Force}}{\text{Surface Tension Force}} \text{ in capillary flows near solid boundaries.}
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\frac{\Delta p}{\frac{1}{2}\rho V^2} = Eu \text{ Euler no.} \propto \frac{\text{Pressure Force}}{\text{Inertial Force}} \text{ important when pressure gradients drive the flow.}
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$$
\frac{p - p_v}{\frac{1}{2}\rho V^2} = C \text{ Cavitation no.} \propto \frac{\text{Pressure Force}}{\text{Inertial Force}} \text{ when pressure drops below vapor pressure.}
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\frac{F_D}{\frac{1}{2}\rho V^2} = C_D \text{ Drag coef.} \propto \frac{\text{Drage Force}}{\text{Inertial Force}} \text{ when drag is important.}
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\frac{\rho V^3}{\mu \omega^2 L} = S_p \text{ Penetration no.} \propto \frac{\text{Time-Dependent Inertial Force}}{\text{Viscous Force}} \text{ Viscous Force}
$$
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$$
\frac{F_D
$$